Modeling the dynamic mode of the chlorinator in the production of chloromethane

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In the production of chloromethane the main apparatus is a chlorinator, which in the production of chloromethane is used directly for chlorination of methane, this procedure requires a clear temperature regime, heating occurs by supplying heating gases from the furnace where the process of burning natural gas in excess air.

The main initial parameter (adjustable value) is the temperature of the reaction gases at the outlet of the chlorinator $\theta out_{p,r}$.

Inlet (control signal, control action) - air flow at the inlet to the furnace G_{nob} . The perturbation is the consumption of reaction gases at the entrance to the apparatus $\theta in_{\text{d.r.}}$.

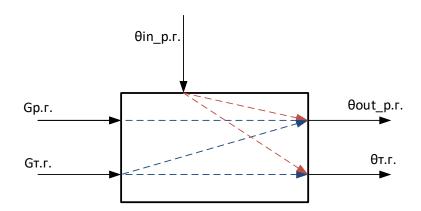


Fig. 1. Structural and parametric scheme of the chlorinator.

 $G_{\mathbf{p},\mathbf{r}}$ – consumption of reaction gases; $\theta in_{\mathbf{p},\mathbf{r}}$ – temperature of reaction gases at the inlet; $\theta out_{\mathbf{p},\mathbf{r}}$ – temperature of reaction gases at the outlet; $G_{\mathbf{r},\mathbf{r}}$ – flue gas consumption; $\theta_{\mathbf{r},\mathbf{r}}$ – temperature of flue gases;

According to the technology of methane chlorination, it is necessary that the temperature of the reaction gases was 450 °C. Temperature control will be carried out through the channel «air flow - outlet temperature of reaction gases».

Equation of heat balances:

$$\begin{cases}
G_{\mathbf{p},\mathbf{r}} \cdot c_{\mathbf{p},\mathbf{r}} \cdot \theta i n_{\mathbf{p},\mathbf{r}} + G_{\mathbf{r},\mathbf{r}} \cdot c_{\mathbf{r},\mathbf{r}} \cdot \theta_{\mathbf{r},\mathbf{r}} + q_r \cdot k \cdot x_b^{\ m} = G_{\mathbf{p},\mathbf{r}} \cdot c_{\mathbf{p},\mathbf{r}} \cdot \theta o u t_{\mathbf{p},\mathbf{r}} \\
G_{\mathbf{n}} \cdot c_{\mathbf{n}} \cdot \theta_{\mathbf{n}} + \alpha \cdot G_{\mathbf{n}o_{\mathbf{B}}} \cdot c_{\mathbf{n}o_{\mathbf{B}}} \cdot \theta_{\mathbf{n}o_{\mathbf{B}}} = G_{\mathbf{r},\mathbf{r}} \cdot c_{\mathbf{r},\mathbf{r}} \cdot \theta_{\mathbf{r},\mathbf{r}}
\end{cases} (1)$$

Table 1 Values of the main static mode

Name	Marking	Numeric value	Dimensionality
Consumption of reaction	$G_{p,r}$	0,5	kg/s
gases			
Flue gas consumption	$G_{\scriptscriptstyle T.\Gamma}$	0,02	kg/s
Fuel consumption	Gπ	0,02	kg/s
Density of flue gases	$ ho_{\scriptscriptstyle \mathrm{T.\Gamma}}$	1,22	kg/m³
Density of reaction gases	$ ho_{\mathrm{p.r}}$	1,4	kg/m³
Reaction gas temperature	$ heta ext{in}_{ ext{p.r}}$	100	°C
(inlet)			
Heat capacity of reaction	С _{р.г}	1.430	kJ / (kg · K)
gases			
Heat capacity of fuel	Сп	2.226	kJ/(kg·K)
Heat capacity of air	Спов	1.007	kJ/(kg·K)
Heat capacity of flue gases	$\mathbf{C}_{\mathrm{T.\Gamma}}$	20.07	kJ/(kg·K)
Energy of activation of a	$\boldsymbol{E}_{\mathrm{a}}$	83.7	kJ
chemical reaction			
Energy is attributed to 1	$q_{\rm r}$	62.31	kJ
mole of substance			
Volume of reaction gases	$V_{\mathrm{p.r}}$	1.5	m ³
Volume of flue gases	$V_{\scriptscriptstyle \mathrm{T.\Gamma}}$	2.5	m ³

From the equation of the second equation of the system (1) we derive the equation of dynamics, where the input parameter is G_{nob} , and the output $-\theta_{\text{T.r.}}$:

$$G_{\Pi} \cdot c_{\Pi} \cdot \theta_{\Pi} + \alpha \cdot G_{\Pi O B} \cdot c_{\Pi O B} \cdot \theta_{\Pi O B} - G_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \theta_{T,\Gamma} = V_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \rho_{T,\Gamma} \frac{d\theta_{T,\Gamma}}{dt}$$
(2)
$$\Delta G_{\Pi} \cdot c_{\Pi} \cdot \theta_{\Pi} + \alpha \cdot \Delta G_{\Pi O B} \cdot c_{\Pi O B} \cdot \theta_{\Pi O B} - G_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \Delta \theta_{T,\Gamma} = V_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \rho_{T,\Gamma} \frac{d\Delta\theta_{T,\Gamma}}{dt}$$
(3)
$$\Delta G_{\Pi} \cdot \frac{c_{\Pi} \cdot \theta_{\Pi}}{G_{T,\Gamma} \cdot c_{T,\Gamma}} + \Delta G_{\Pi O B} \cdot \frac{\alpha \cdot c_{\Pi O B} \cdot \theta_{\Pi O B}}{G_{T,\Gamma} \cdot c_{T,\Gamma}} = \frac{V_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \rho_{T,\Gamma}}{G_{T,\Gamma} \cdot c_{T,\Gamma}} \cdot \frac{d\Delta\theta_{T,\Gamma}}{dt} + \Delta\theta_{T,\Gamma}$$
(4)
$$T1 = \frac{V_{T,\Gamma} \cdot c_{T,\Gamma} \cdot \rho_{T,\Gamma}}{G_{T,\Gamma} \cdot c_{T,\Gamma}} \quad k_{Gt_\theta tg} = \frac{c_{\Pi} \cdot \theta_{\Pi}}{G_{T,\Gamma} \cdot c_{T,\Gamma}} \quad k_{Gair_\theta tg} = \frac{\alpha \cdot c_{\Pi O B} \cdot \theta_{\Pi O B}}{G_{T,\Gamma} \cdot c_{T,\Gamma}}$$
(5)

Equations in canonical form

$$k_{Gt_\theta tg} \Delta G_{\Pi} + k_{Gair_\theta tg} \Delta G_{\Pi OB} = T1 \frac{d\Delta \theta_{T,\Gamma}}{dt} + \Delta \theta_{T,\Gamma} \quad (6)$$

Perform the transformation of equation (6) according to Laplace

$$\theta_{\text{\tiny T.\Gamma}} = \frac{k_{Gair_\theta tg} \Delta G_{\text{\tiny NOB}}}{T1 \cdot n + 1} \tag{7}$$

Substituting in the first equation of the system (1) equation (7) we derive the equation of dynamics, where the input parameter is

 G_{nob} , and the output $-\theta out_{\text{p.r}}$:

$$G_{\mathbf{p},\mathbf{r}} \cdot \mathbf{c}_{\mathbf{p},\mathbf{r}} \cdot \theta i n_{\mathbf{p},\mathbf{r}} + G_{\mathbf{T},\mathbf{r}} \cdot \mathbf{c}_{\mathbf{T},\mathbf{r}} \cdot \theta_{\mathbf{T},\mathbf{r}} + q_r \cdot k \cdot x_b{}^m - G_{\mathbf{p},\mathbf{r}} \cdot \mathbf{c}_{\mathbf{p},\mathbf{r}} \cdot \theta out_{\mathbf{p},\mathbf{r}} = V_{\mathbf{p},\mathbf{r}} \cdot \mathbf{c}_{\mathbf{p},\mathbf{r}} \cdot \mathbf{c}$$

$$k = A \cdot e^{-\frac{E_{a}}{R \cdot \theta out_{p,r}}} \quad (9)$$

$$y = G_{p,r} \cdot c_{p,r} \cdot q_{r} \cdot A \cdot E_{a} \frac{e^{\frac{E_{a}}{R \cdot \theta out_{p,r}}}}{e^{\frac{E_{a}}{R \cdot \theta out_{p,r}}}} \quad (10)$$

$$\frac{G_{p,r} \cdot c_{p,r}}{y} \cdot \Delta \theta i n_{p,r} + \frac{G_{r,r} \cdot c_{r,r}}{y} \cdot \Delta \theta_{r,r} = \frac{V_{p,r} \cdot c_{p,r} \cdot \rho_{p,r}}{y} \frac{d\Delta \theta out_{p,r}}{dt} + \Delta \theta out_{p,r} \quad (11)$$

$$k_{\theta i n_{r}} = \frac{G_{p,r} \cdot c_{p,r}}{y} \quad k_{\theta out_{r}} = \frac{G_{r,r} \cdot c_{r,r}}{y} \quad T2 = \frac{V_{p,r} \cdot c_{p,r} \cdot \rho_{p,r}}{y} \quad (12)$$

Equations in canonical form

$$k_{\theta in_G} \cdot \Delta \theta in_{p.r} + k_{\theta out_tg} \cdot \Delta \theta_{r.r} = T2 \frac{d\Delta \theta out_{p.r}}{dt} + \Delta \theta out_{p.r}$$
(13)

Perform the transformation of equation (13) according to Laplace

$$(T2 \cdot p + 1)\Delta\theta out_{p,r} = \frac{k_{\theta out_tg} \cdot k_{Gair_\theta tg}}{(T1 \cdot p + 1)} \Delta G_{\text{nob}}$$

$$\frac{\theta out_{p,r}(p)}{\Delta G_{\text{nog}}(p)} = \frac{k_{\theta out_tg} \cdot k_{Gair_\theta tg}}{(T1 \cdot p + 1)(T2 \cdot p + 1)}$$

$$(15)$$

According to the results of the transformations, the transfer function of the system via the control channel «air flow - the temperature of the reaction gases at the outlet» was obtained.

$$W(p) = \frac{k_{\theta out_tg} \cdot k_{Gair_\theta tg}}{(T1 \cdot p + 1)(T2 \cdot p + 1)}$$
 (16)

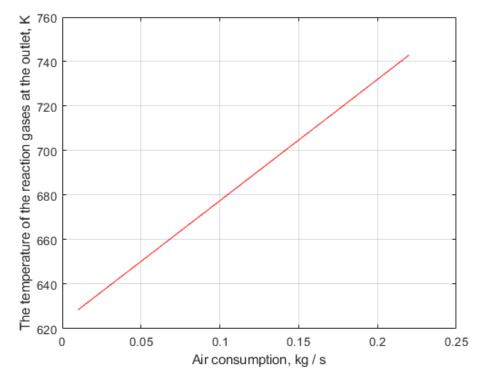


Fig. 2 Static characteristic on the channel $G_{\text{nob}} \to \theta out_{\text{p.r.}}$

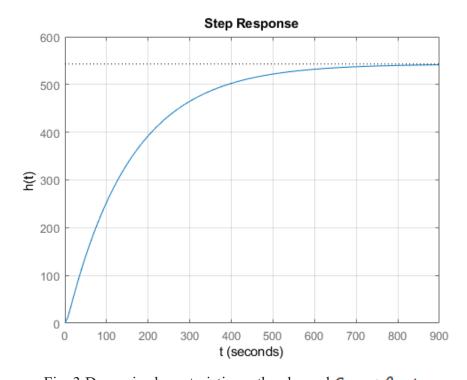


Fig. 3 Dynamic characteristic on the channel $G_{\text{nob}} \to \theta out_{\text{p.r}}$

Literature

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